

# Simple rules-of-thumb for ice fall/throw safety distances

Alexander Stökl & Andreas Krenn  
Energiewerkstatt e.V., Austria

**energiewerkstatt**<sup>o</sup>  
VEREIN & TECHNISCHES BÜRO FÜR ERNEUERBARE ENERGIE

 Federal Ministry  
Republic of Austria  
Transport, Innovation  
and Technology

**IEA** FORSCHUNGS  
KOOPERATION

# Scope

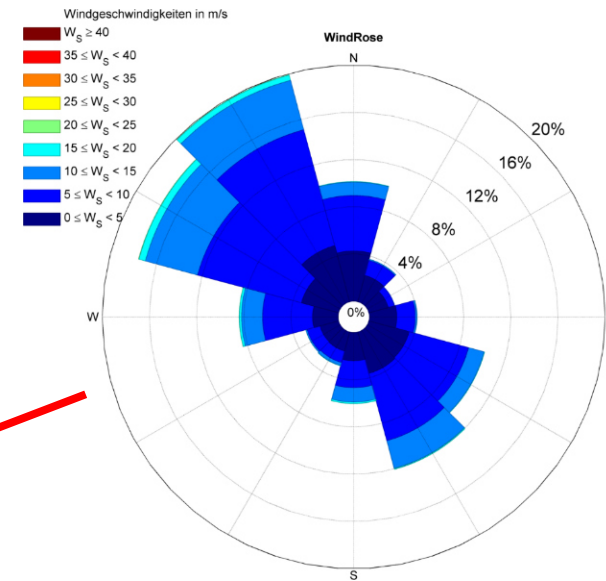
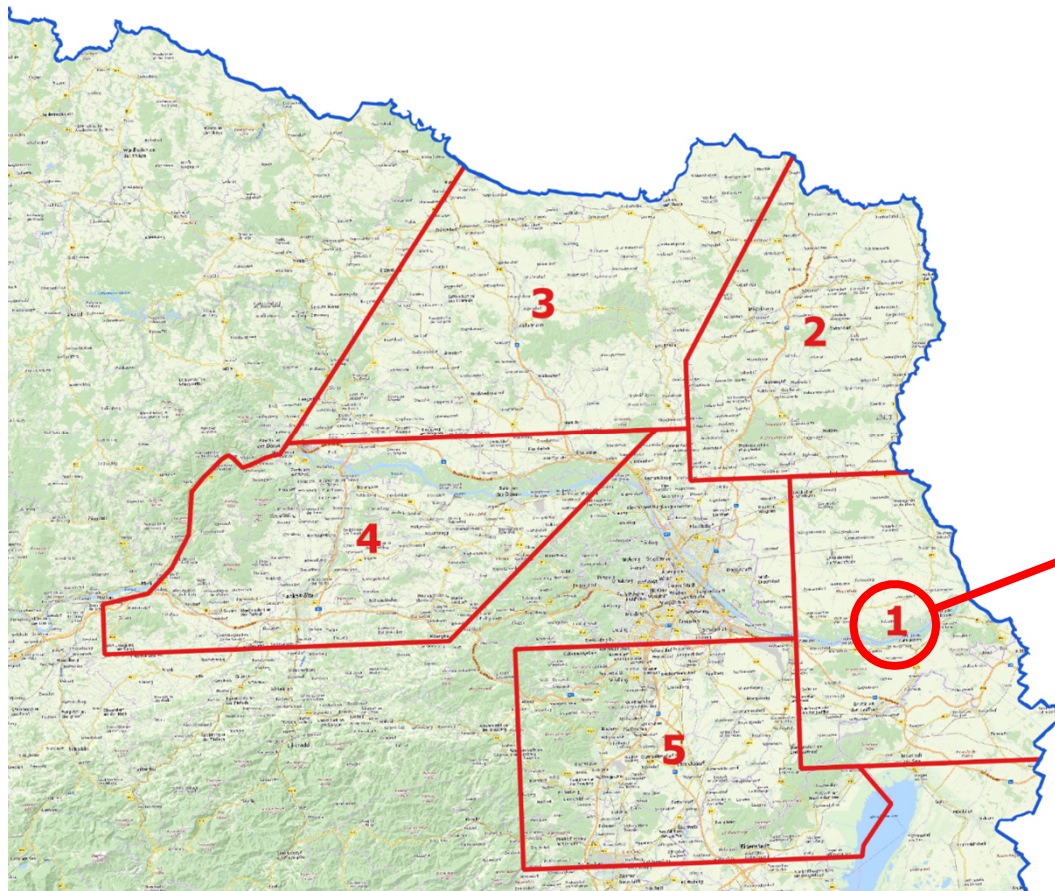
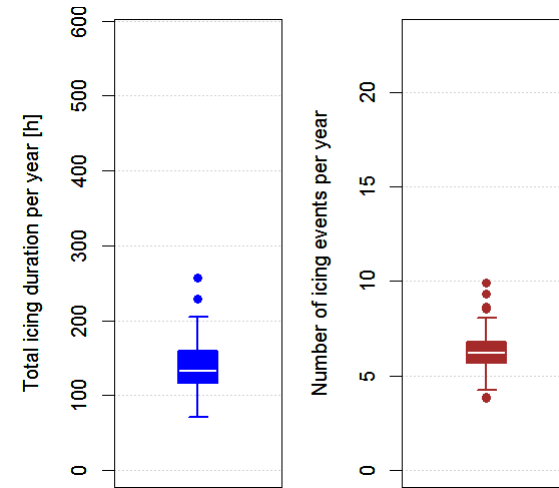
- This is a H&S presentation
- In Austria (as well as some countries) icing is first and foremost a H&S issue and icing losses are only of secondary importance
- Builds on a previous study in Austria
- And based on the conviction that, to be useful, any advise should be as simple as possible

# Austrian Project: R.Ice 'Risk Analysis of Wind Turbine Icing'

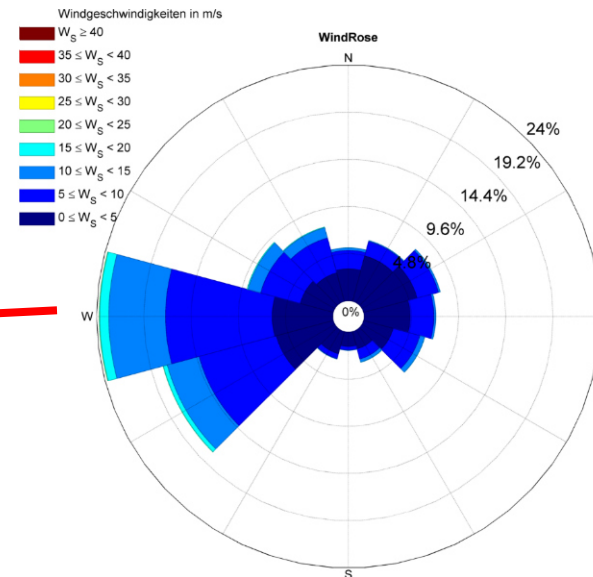
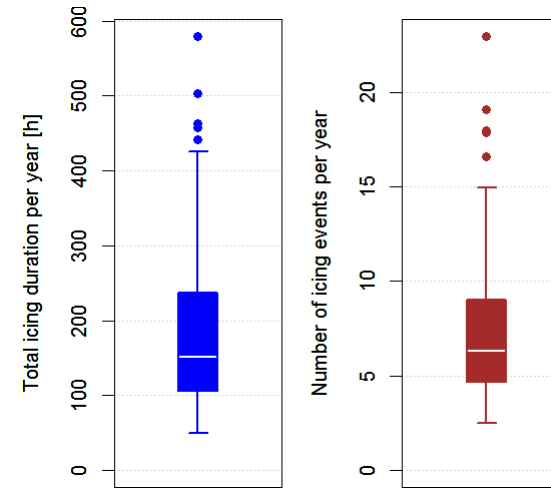
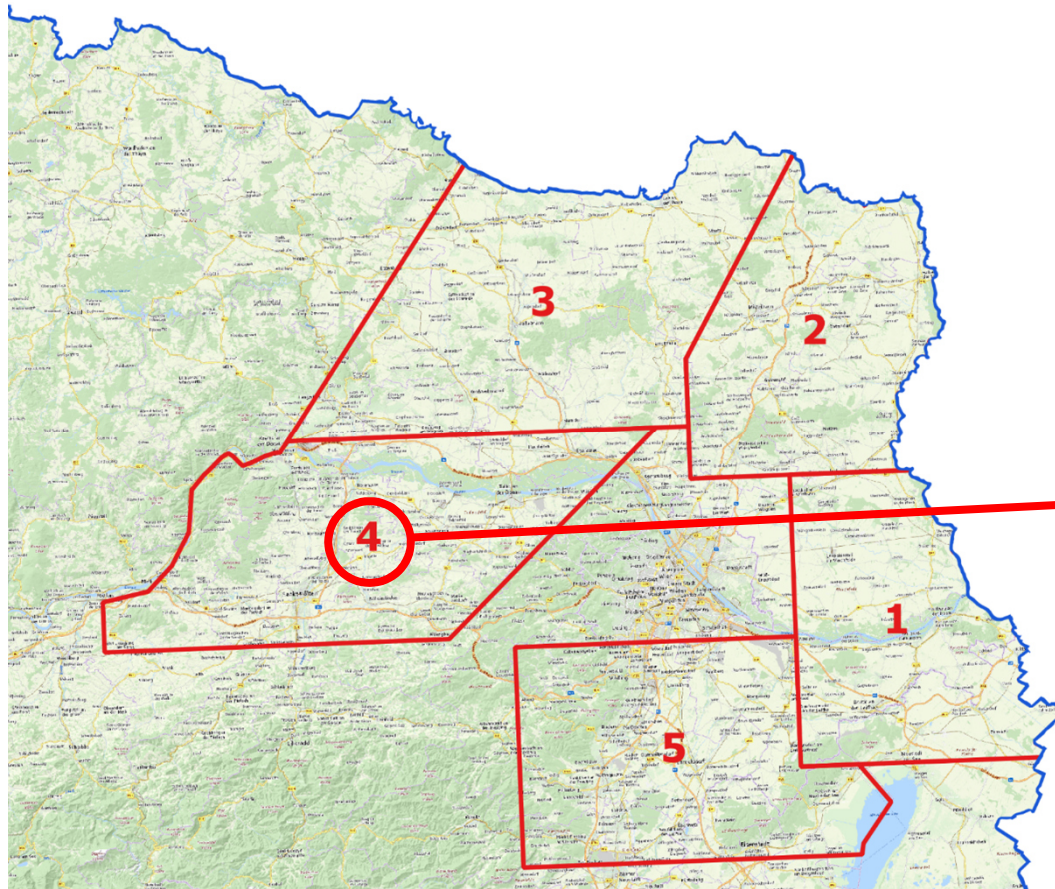
- Part of this was presented on Winterwind 2019
- Looked at five more or less homogeneous regions in Eastern Austria
- Averaged wind- and icing-conditions



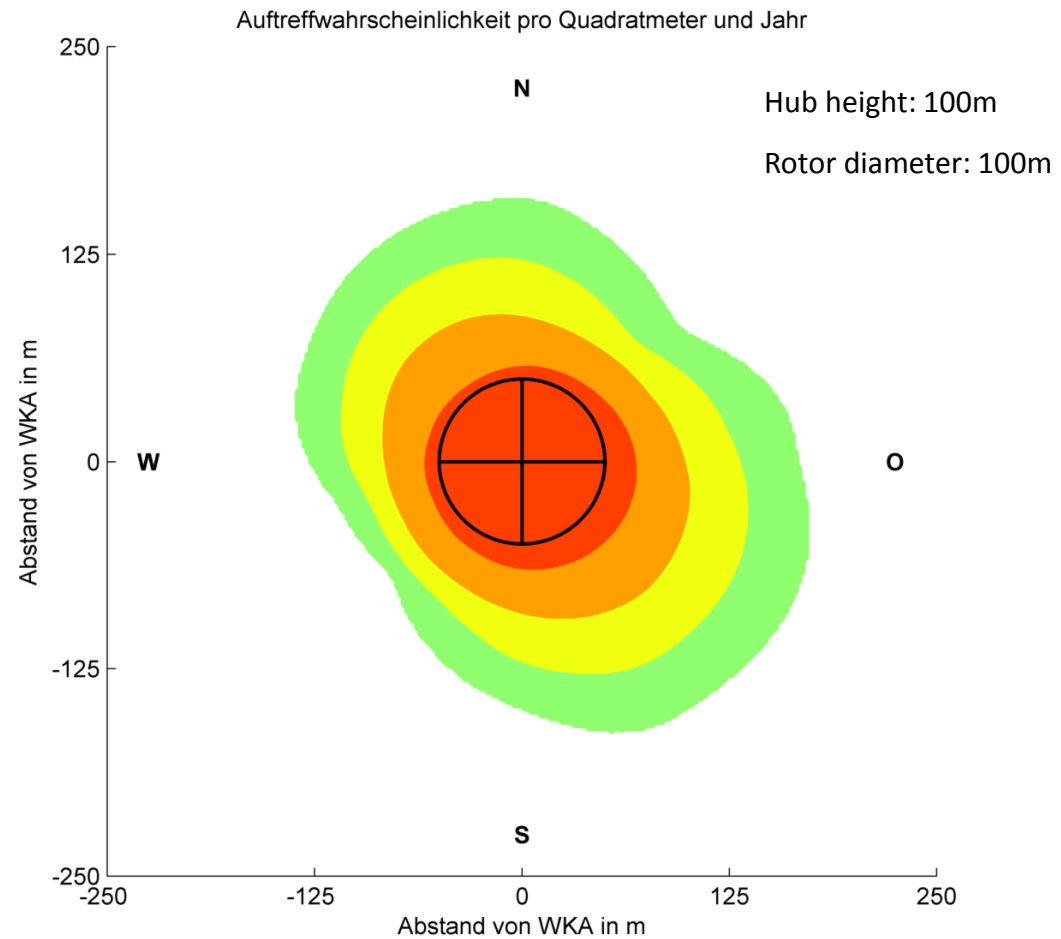
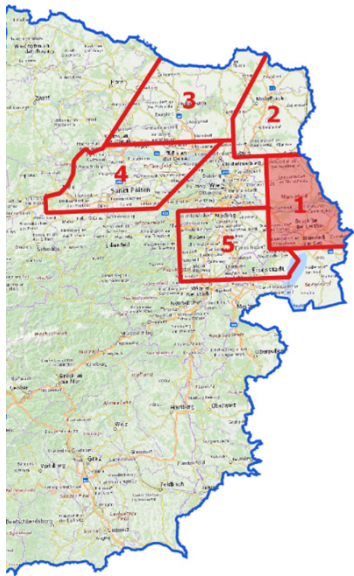
# Region-wise wind- and icing conditions...



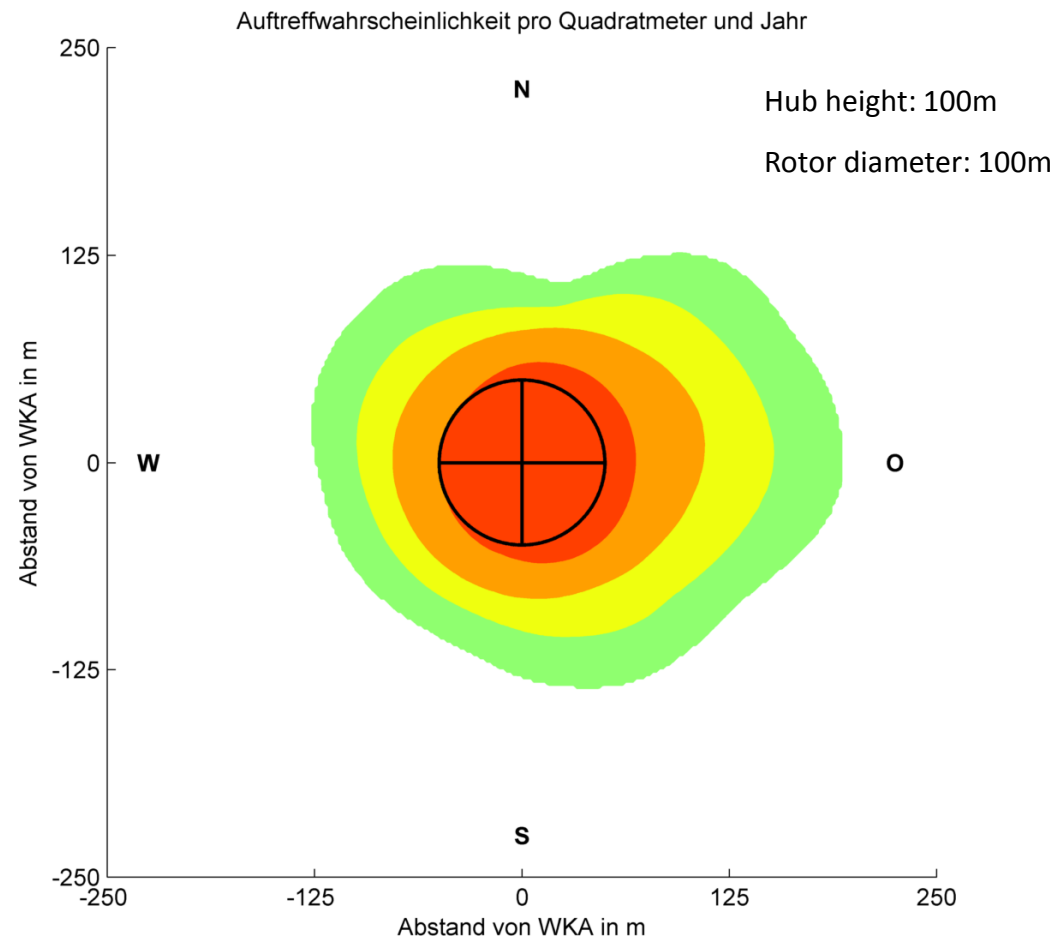
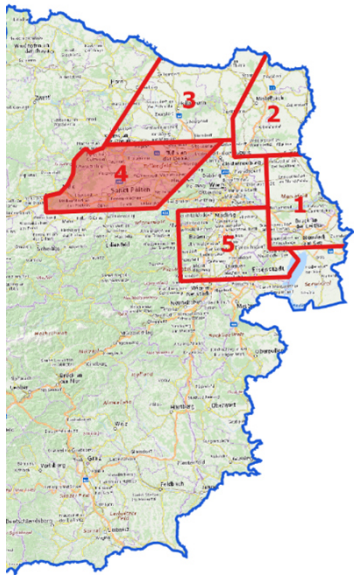
# Region-wise wind- and icing conditions...



## ... lead to region-wise impact distributions



## ... lead to region-wise impact distributions



## Limits and stand-off radii

Considering two limits for the yearly impact probability:

- **$10^{-3} \text{ m}^{-2} \text{ year}^{-1}$**  for non-critical infrastructure and usage scenarios (also used for ice fall warning signs/warning lights), e.g.:
  - Unspecified activities up to, on average, 0,5h per day (indiv.)
  - Pedestrian, jogger, biker, on average, once per day (indiv.)
  - Vehicles dirt/forest road, twice per day (indiv.), 200 per day (coll.)
  - Hiking/biking path, 500 per day (coll.)
- **$10^{-5} \text{ m}^{-2} \text{ year}^{-1}$**  corresponds to a LIRA (localized individual risk)  $< 10^{-6}$ 
  - Ice fall risk is no concern
  - Fine to have public roads, railways, leisure areas, settlements, etc.

Based on accepted risk levels of  $10^{-6} \text{ year}^{-1}$  individual and  $10^{-4} \text{ year}^{-1}$  collective (IEA Task 19 recommendations)

Either extreme assumptions or with a safety factor of 10 or greater

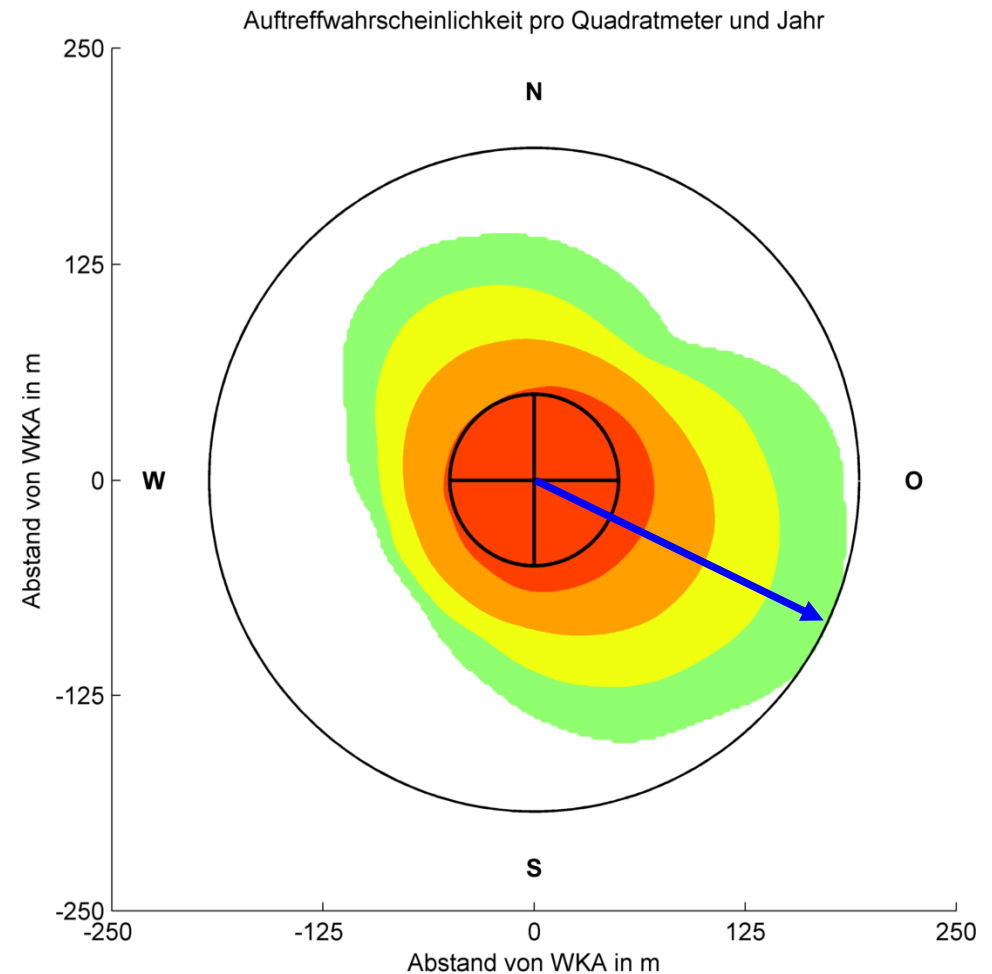
Everything on average during icing season



To simplify matters:  
only considering the **maximum over all directions**

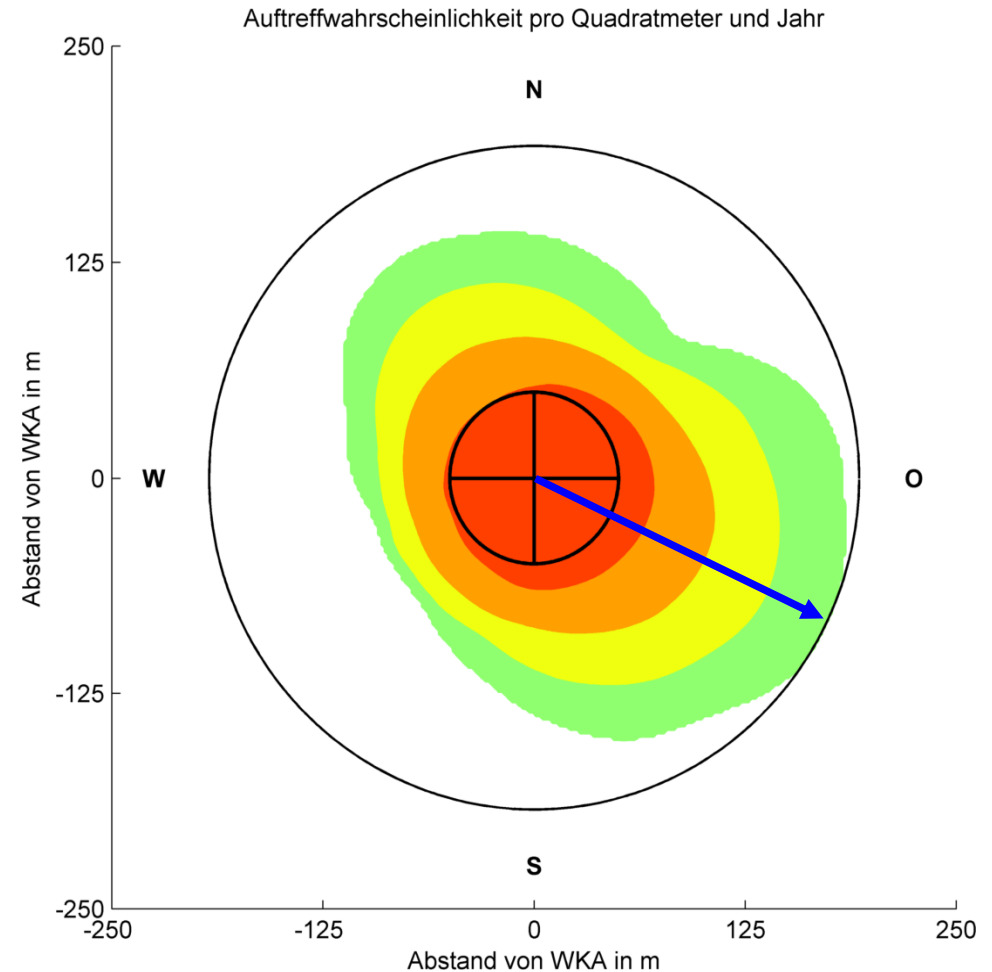
- It turns out (as we will see later) that the blade tip height is the relevant reference
- Leads to standoff radii in units of the blade tip height:

| Level # yr <sup>-1</sup> m <sup>-2</sup> | 10 <sup>-3</sup> | 10 <sup>-5</sup> |
|--|------------------|------------------|
| Region 1                                 | 0,74             | 1,27             |
| Region 2                                 | 0,74             | 1,28             |
| Region 3                                 | 0,69             | 1,18             |
| Region 4                                 | 0,78             | 1,36             |
| Region 5                                 | 0,78             | 1,34             |



To simplify matters:  
only considering the **maximum over all directions**

- **For ice fall (WT Stopped)**  
The maximum distance is determined by the wind direction with the highest wind speed and the frequency of occurrence in that bin.
- **For ice throw (WT operating)**  
Things are not quite as straightforward and require a short discussion...



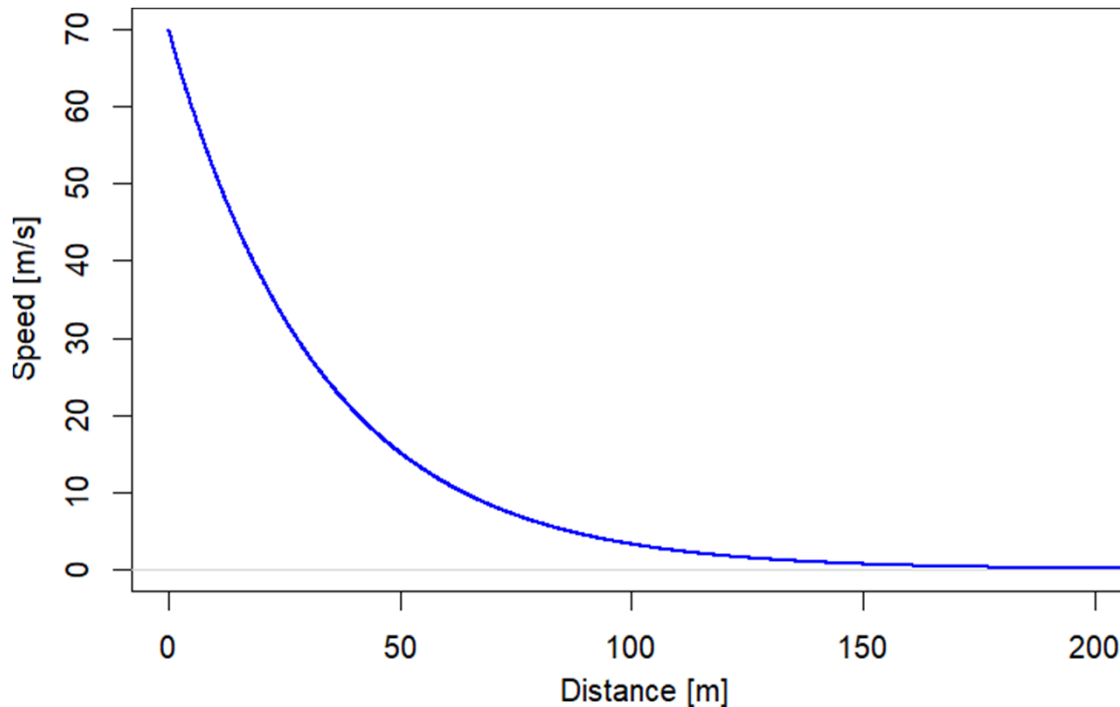
## Stopping length and turbine size

Equation of motion for an ice piece in one DOF:

$$\frac{1}{2}\rho u^2 C_D A/m = -a = -\frac{\partial u}{\partial t}$$

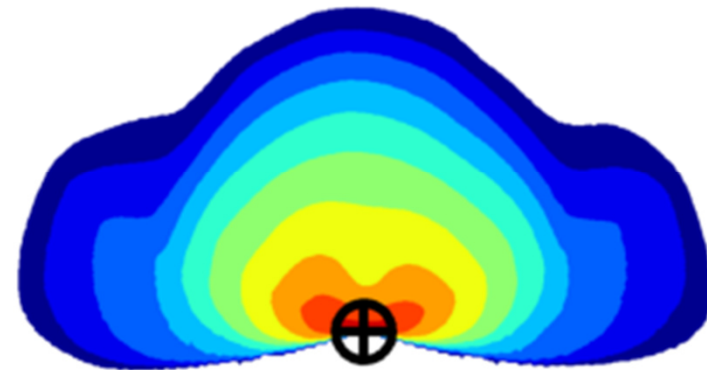
Has the solution

$$u = u_0 \cdot e^{-\frac{x}{l_{\text{stop}}}} \quad \text{with stopping length} \quad \frac{1}{l_{\text{stop}}} = \frac{1}{2}\rho C_D A/m$$



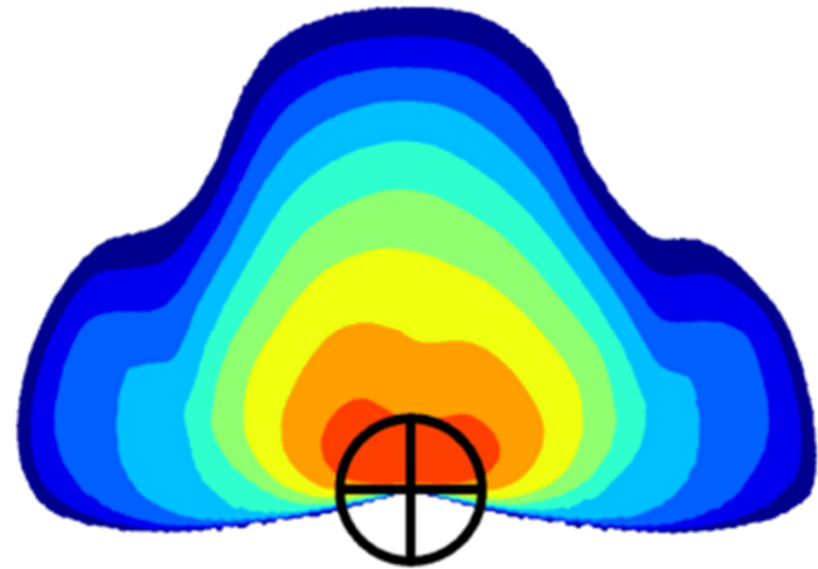
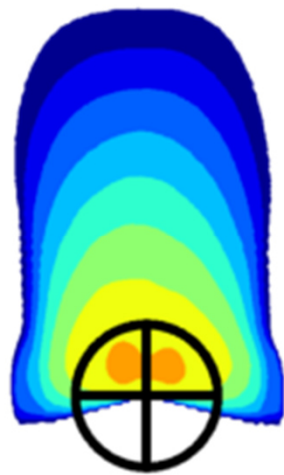
$$\begin{aligned} u_0 &= 70 \text{ m/s} \\ \rho &= 1,225 \text{ kg/m}^3 \\ C_D &= 1 \\ A/m &= 0,05 \text{ m}^2/\text{kg} \\ l_{\text{stop}} &\approx \mathbf{33\text{m}} \end{aligned}$$

**Regardless of  
turbine size!!**



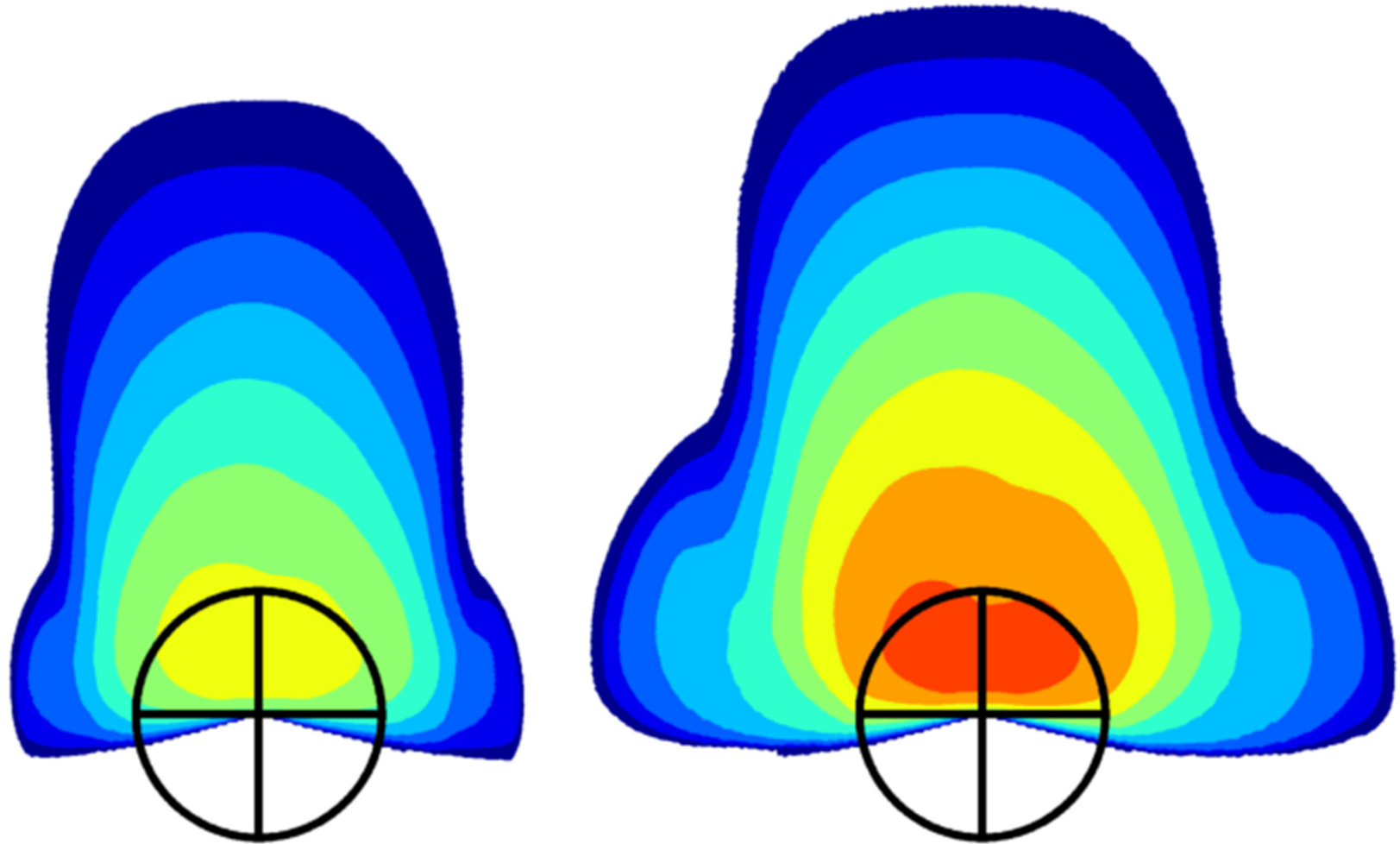
Dia: 40m HH: 40m TH: 60m

$V_{avg}$ : 10 m/s



Dia: 100m HH: 100m TH: 150m

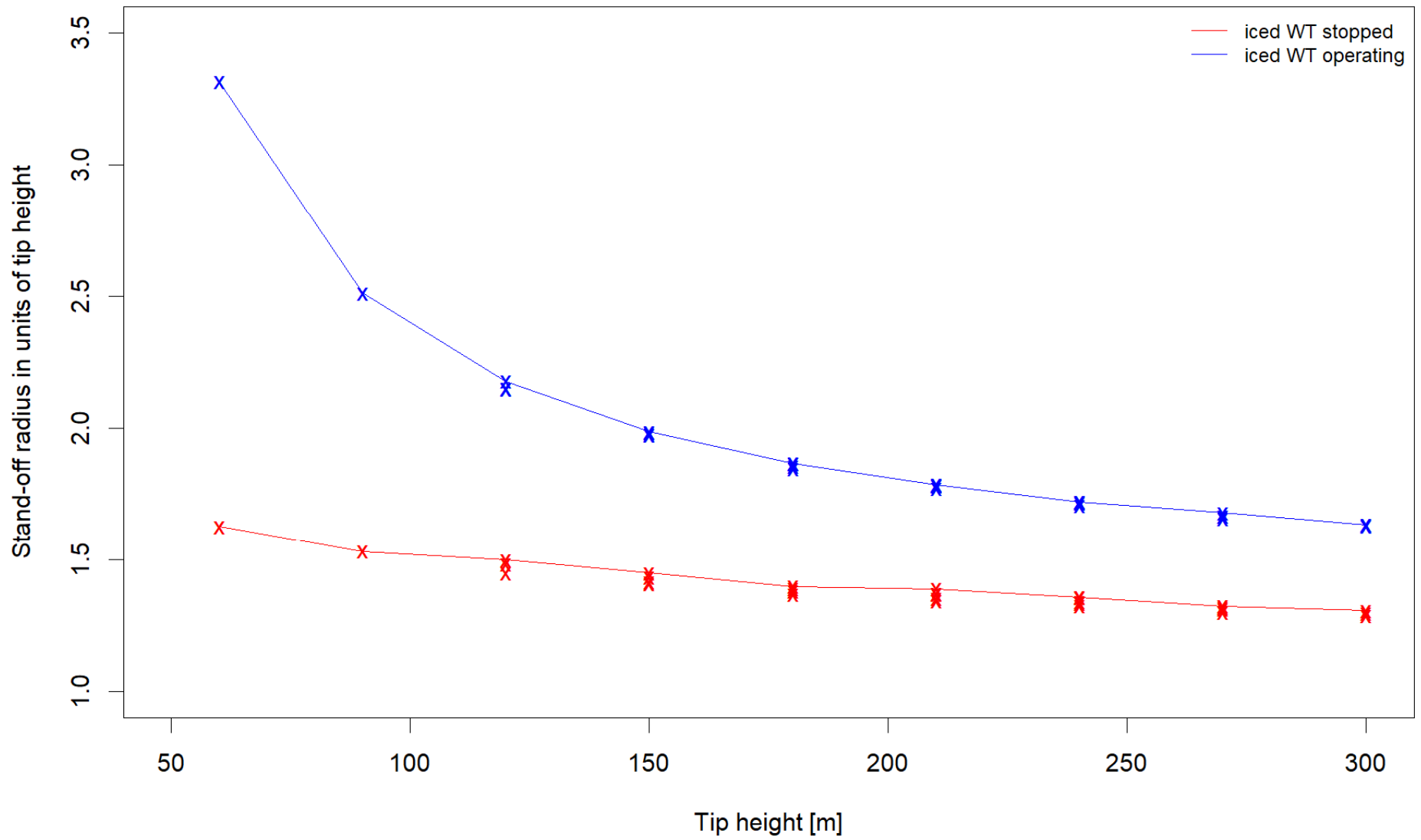
$V_{avg}$ : 10 m/s



Dia: 200m HH: 200m TH: 300m

$V_{avg}$ : 10 m/s

Stand-off radius for a impact density of  $10^{-5}$ ,  $V_{avg} = 10$  m/s



# Procedure in this study

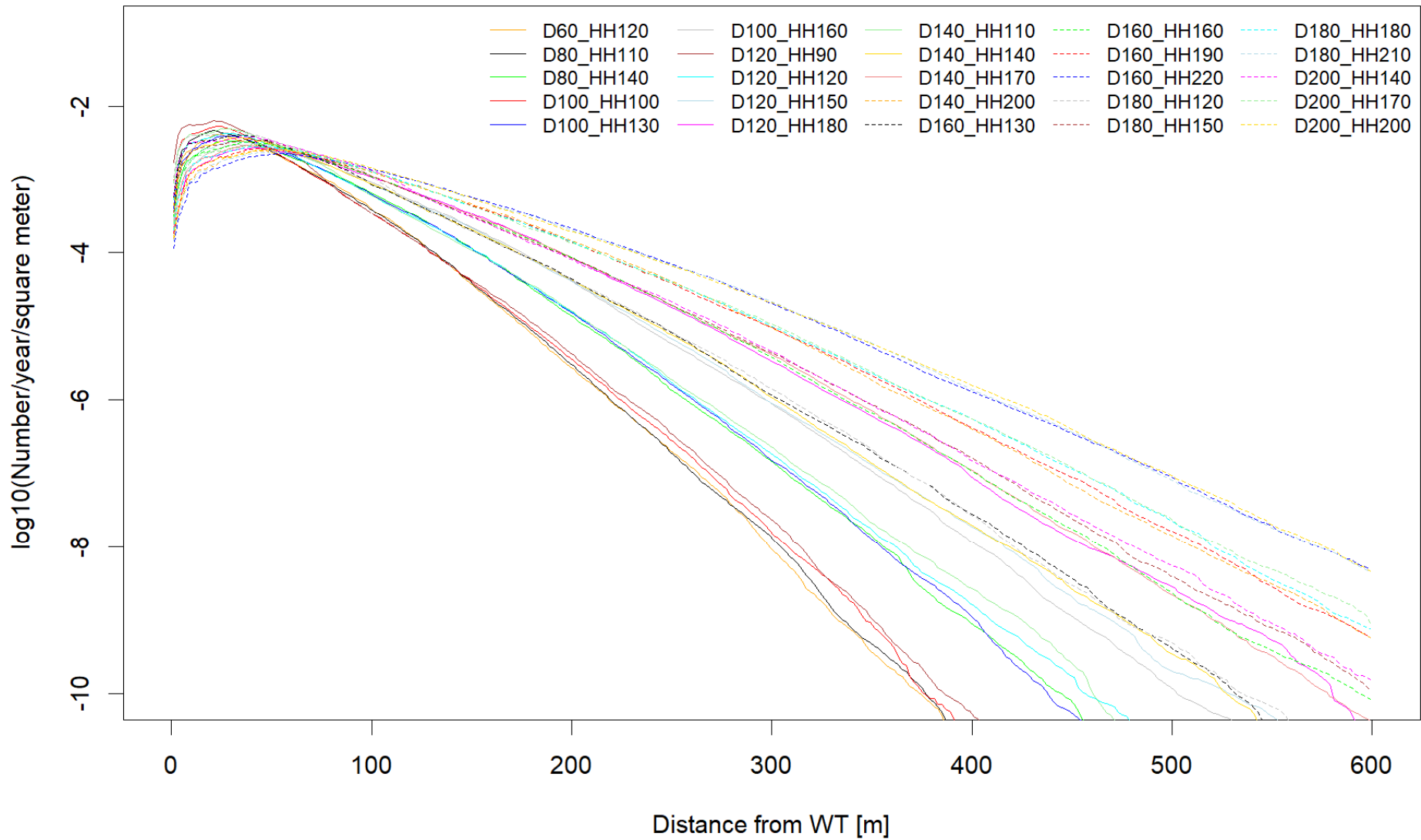
- Take reference to the average wind speed in the „worst bin“: from 7 m/s to 15 m/s
- Wind turbines from 150m to 300m tip height in 25 different configurations
- For IEA icing classes 1 to 5
- Considering ice throw and ice fall



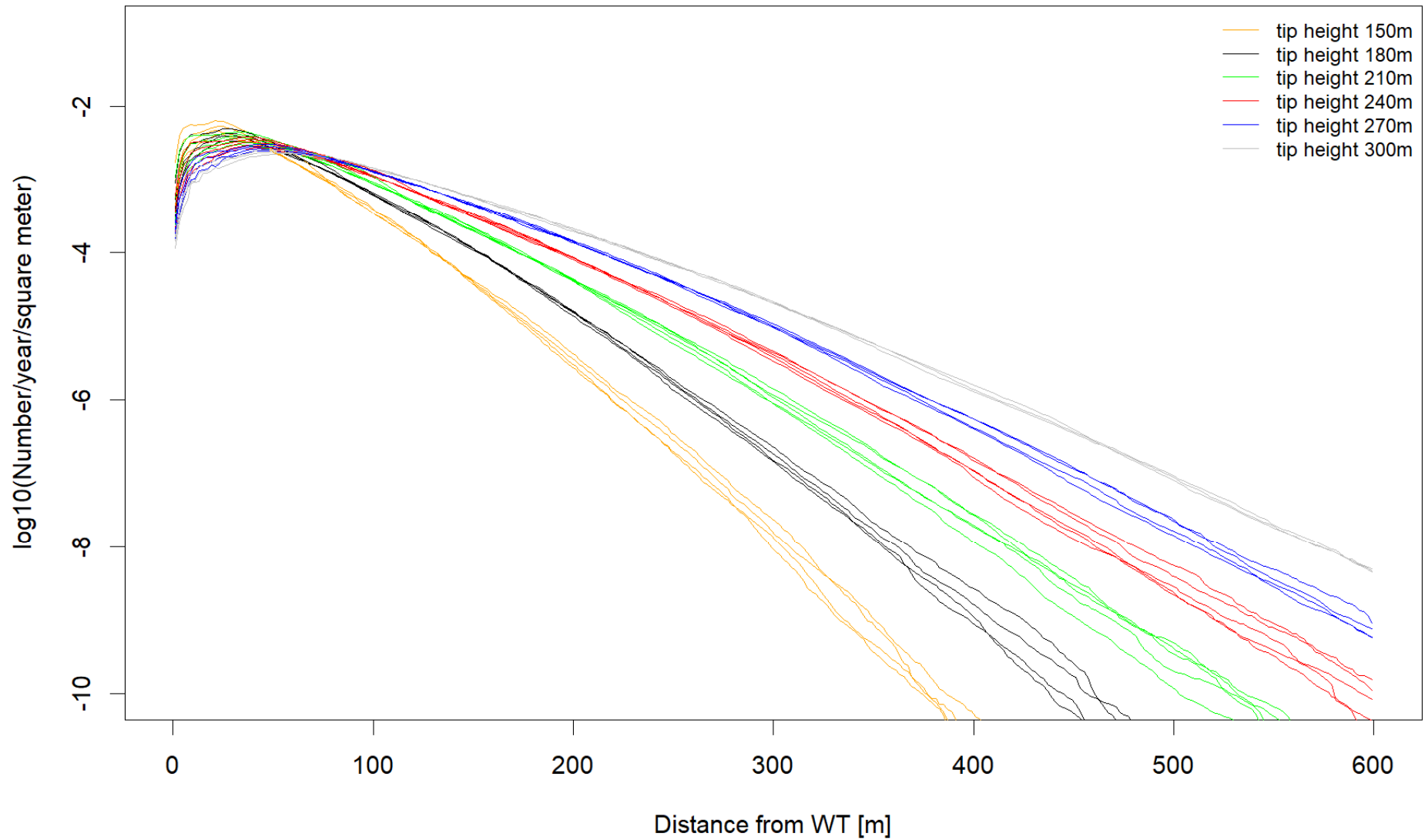
# Technicalities & Assumptions

- WT operation: cut-in 3 m/s, rated 12 m/s, cut-out 25 m/s
- Spectrum of ice pieces in A/m, according to Task 19 ice fall recommendations
- Ice pieces above 100g are considered potentially lethal
- Number of ice pieces according to Task 19 ice fall recommendations and scaled with turbine size
- Factor of 10 for the number of ice pieces between standstill and in-operation
- Wind speed defined at hub height, Rayleigh distribution, wind shear with  $\alpha=2$
- Binning in 12 wind directions

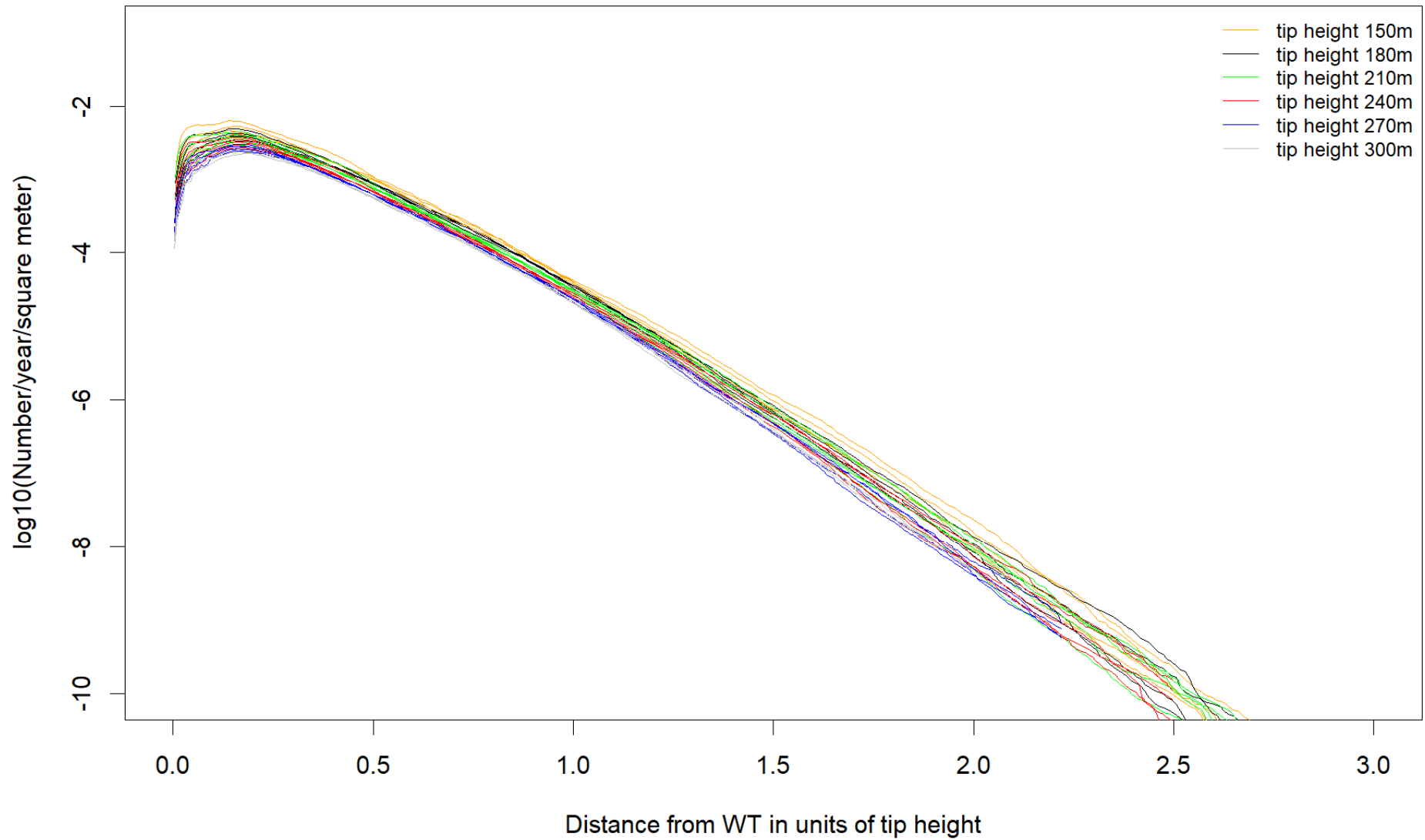
### Impact probability of ice pieces, maximum over all directions, mean wind = 8 m/s



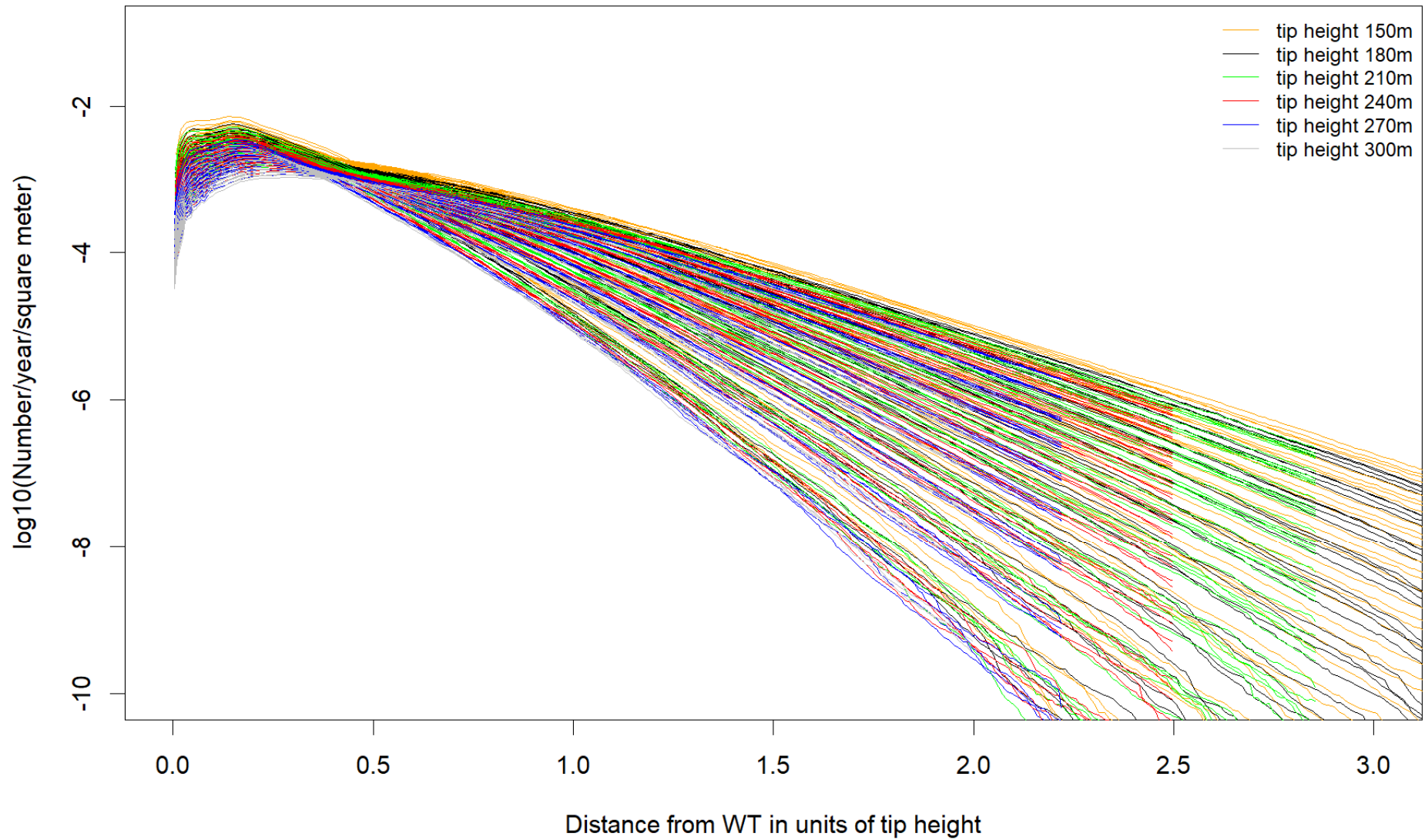
### Impact probability of ice pieces, maximum over all directions, mean wind = 8 m/s



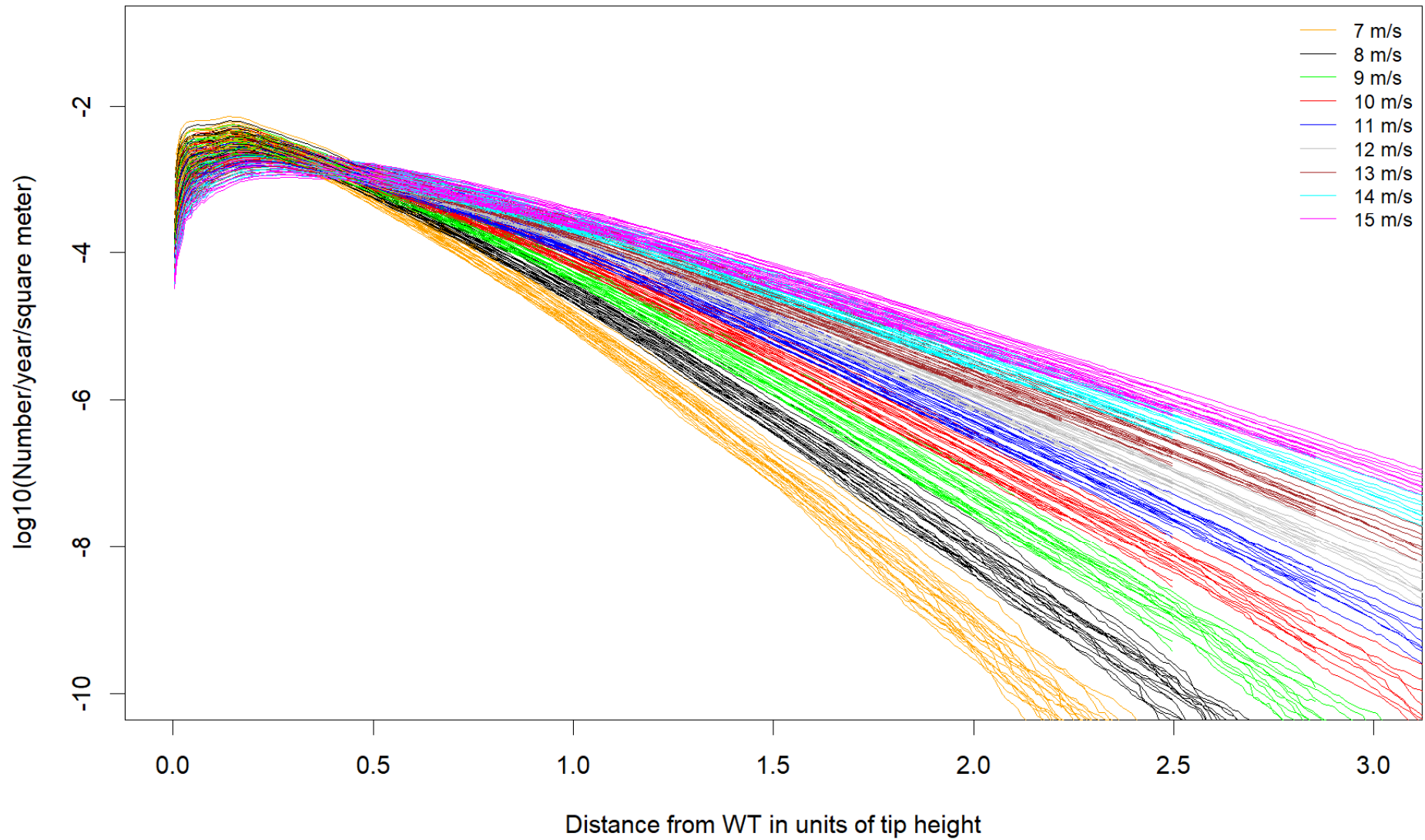
### Impact probability of ice pieces, maximum over all directions, mean wind = 8 m/s



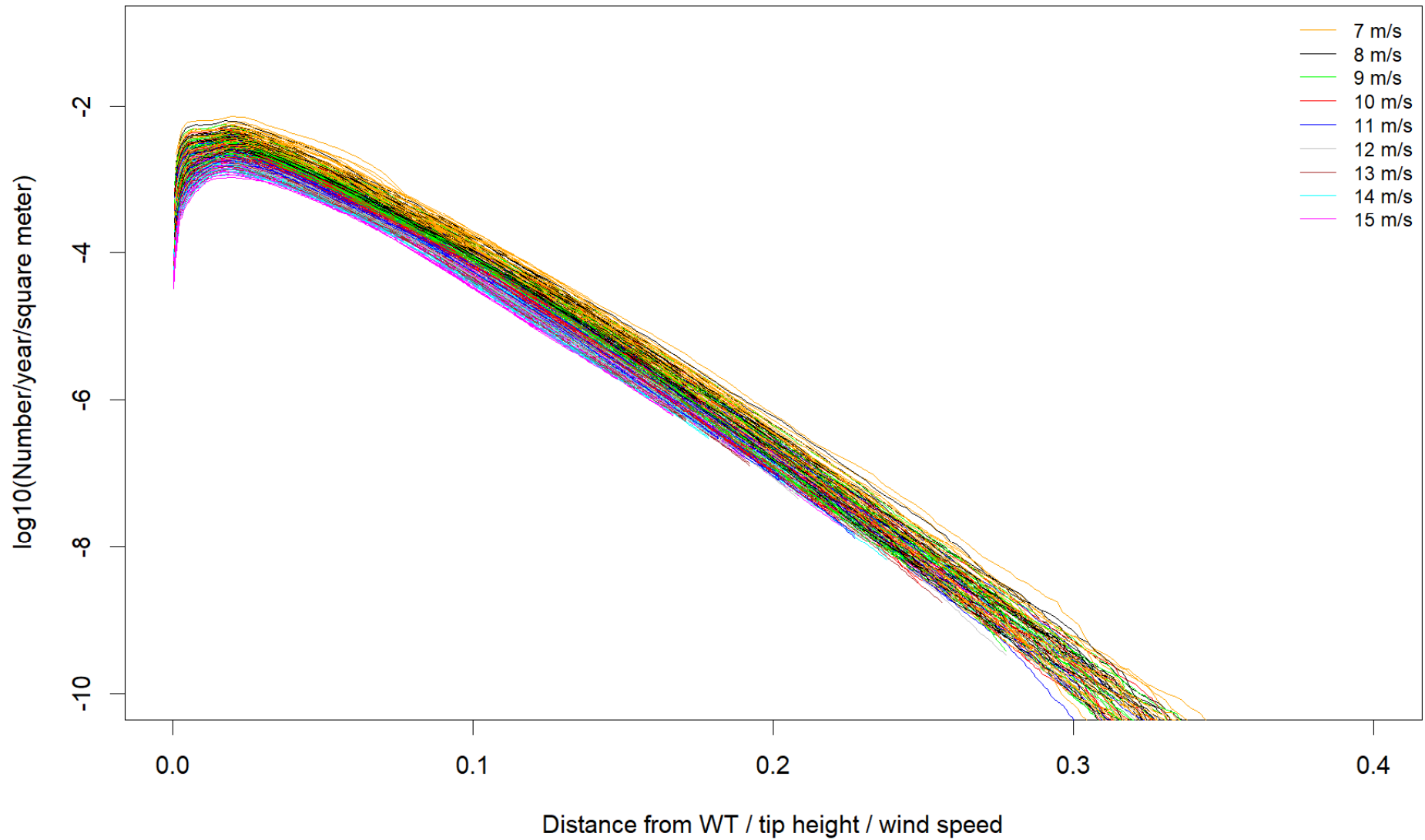
## Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



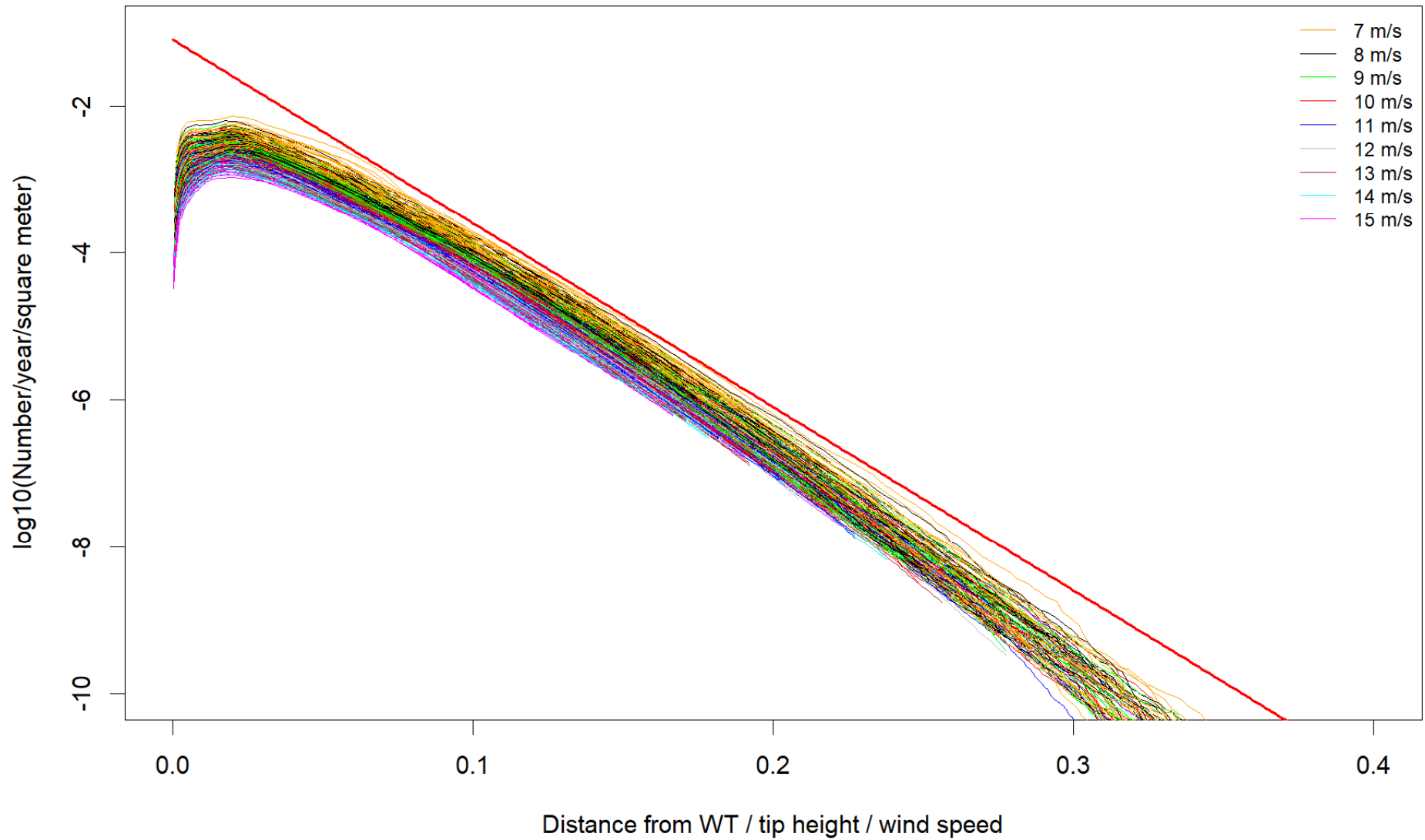
### Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



### Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s

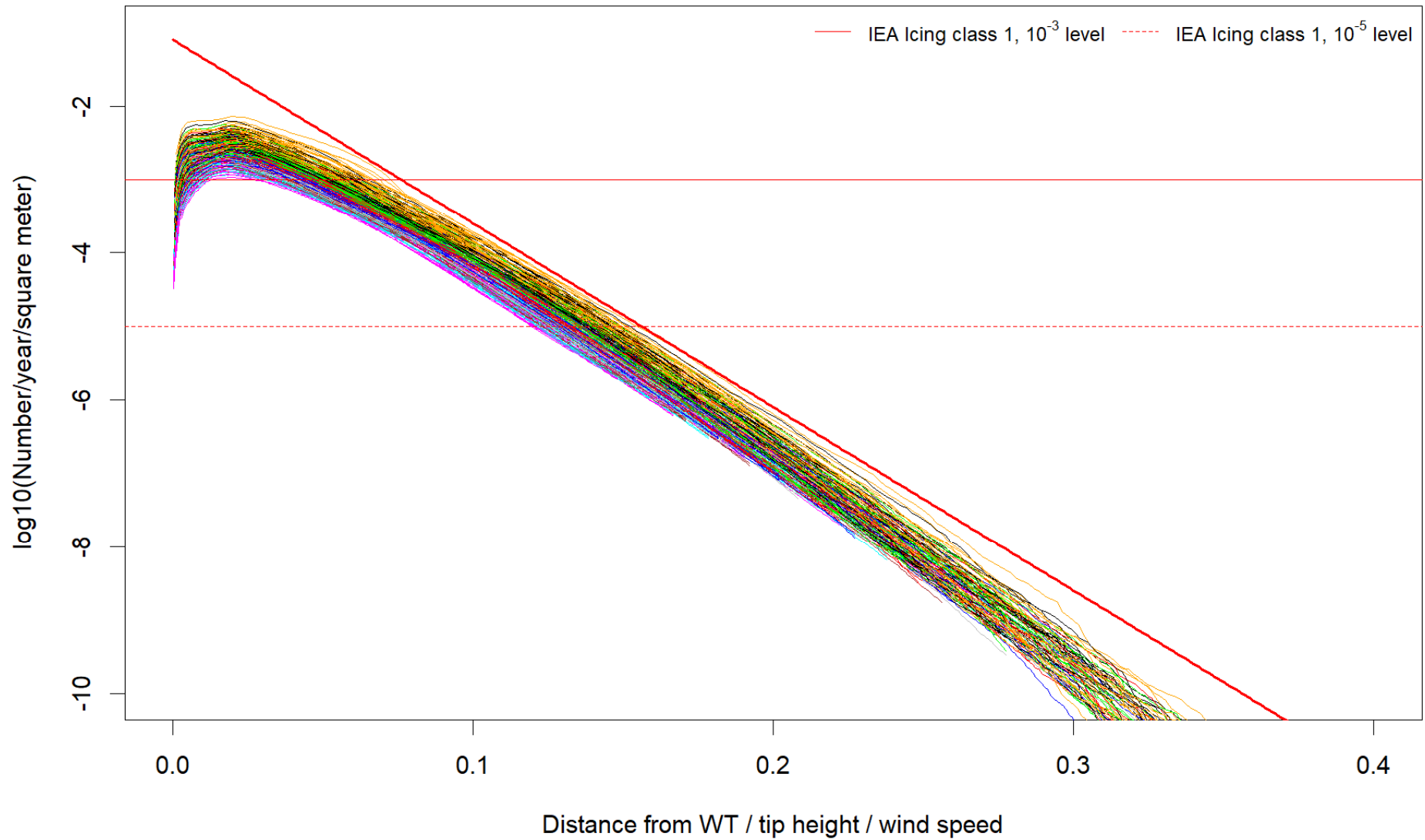


### Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s

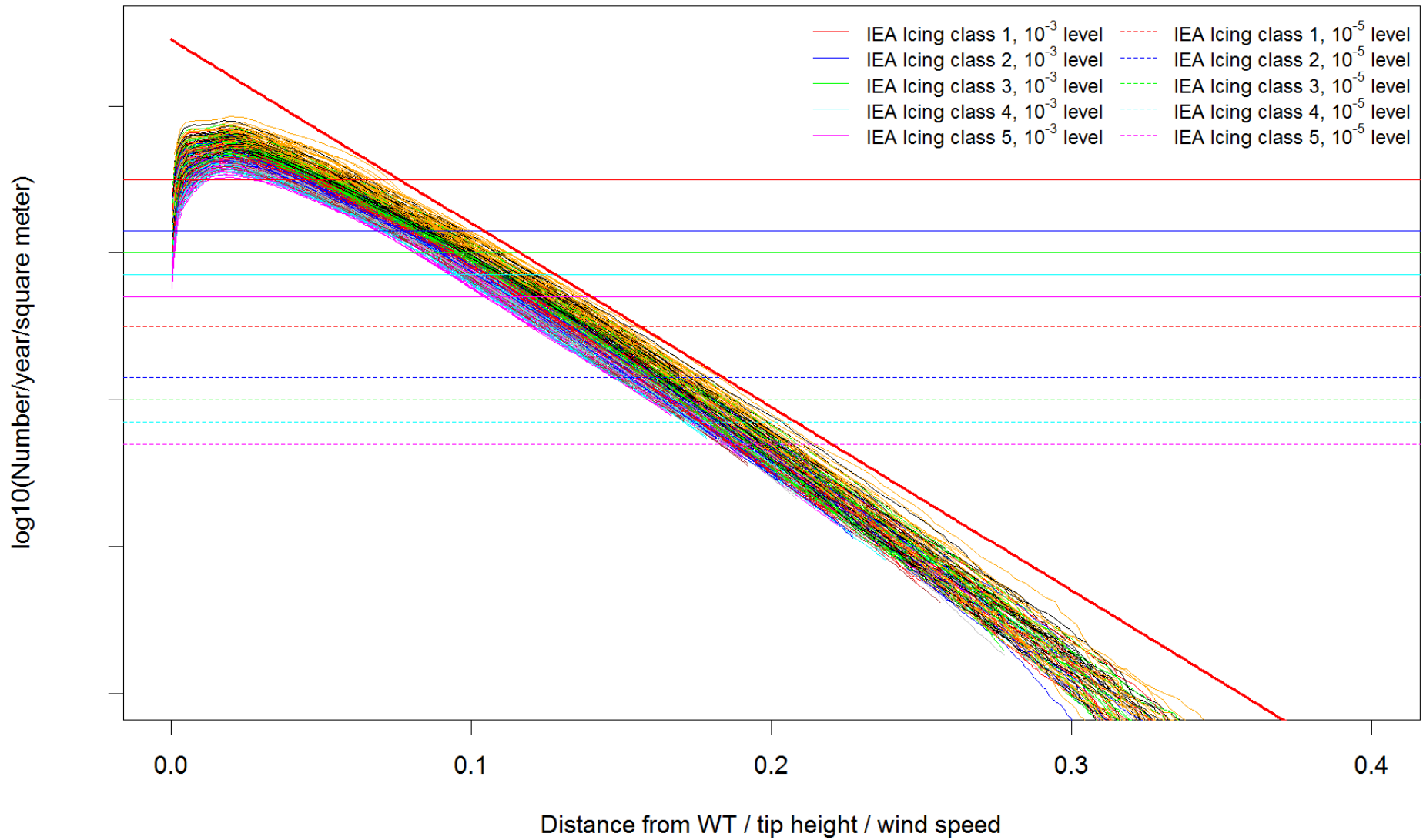




# Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



# Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



## Formulae for stand-off radii: iced WT stopped

- **$10^{-3} \text{ m}^{-2} \text{ year}^{-1}$**  for non-critical infrastructure and usage scenarios  
(also used for ice fall warning signs/warning lights)

$$\frac{R_{\min}}{TH} = V_{\text{avg}} \frac{3 + \log(a) + \log(b) - 1.1}{25}$$

**$10^{-5} \text{ m}^{-2} \text{ year}^{-1}$**  corresponds to a LIRA (localized individual risk)  $< 10^{-6}$ , i.e. ice fall risk is no concern

$$\frac{R_{\min}}{TH} = V_{\text{avg}} \frac{5 + \log(a) + \log(b) - 1.1}{25}$$

$$a = \begin{cases} 1 & \text{for IEA icing class 1} \\ 5 & \text{for IEA icing class 2} \\ 10 & \text{for IEA icing class 3} \\ 20 & \text{for IEA icing class 4} \\ 40 & \text{for IEA icing class 5} \end{cases}$$

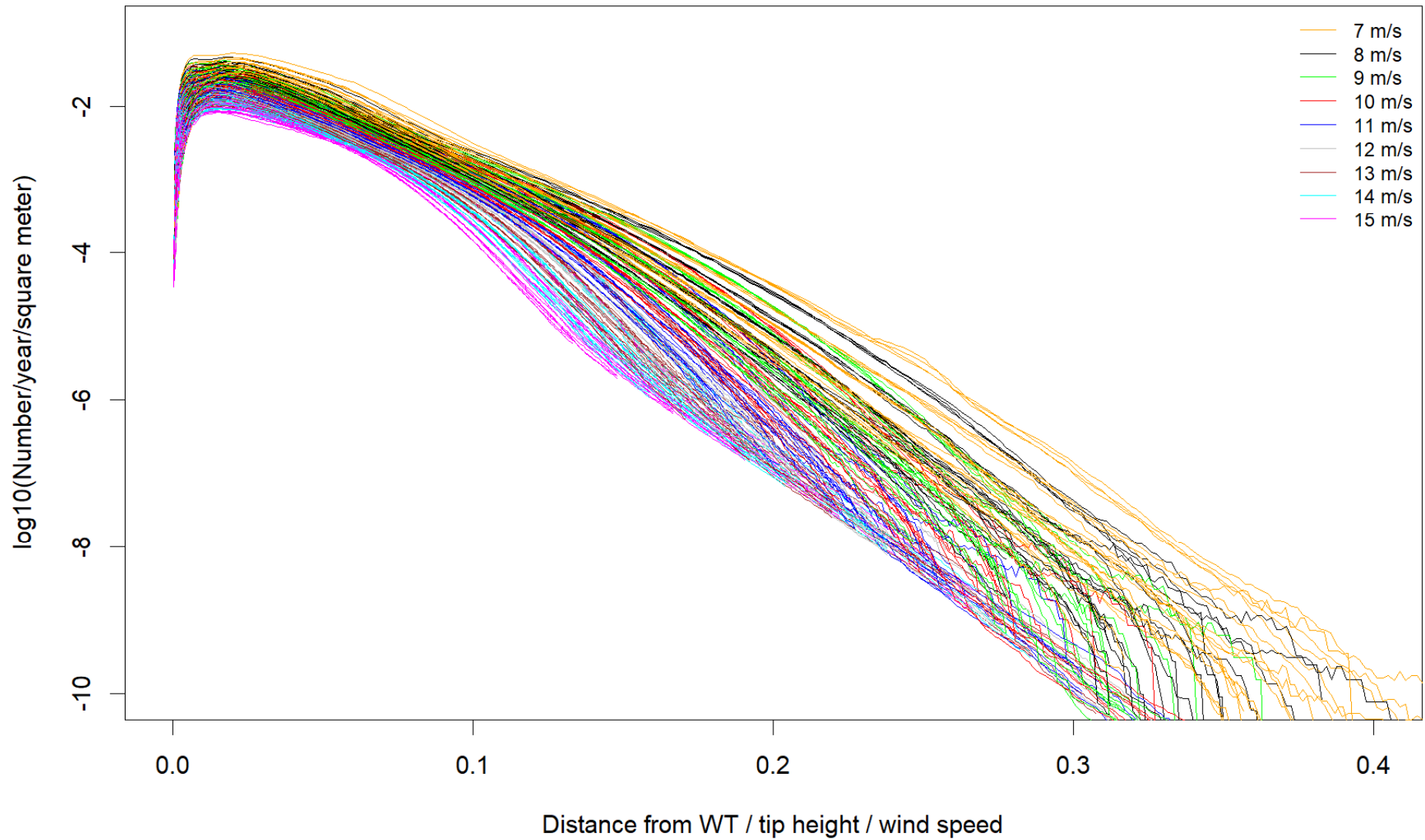
$$b = \max(1, P_{\text{bin}} \cdot 12)$$

$TH$  ... tip height

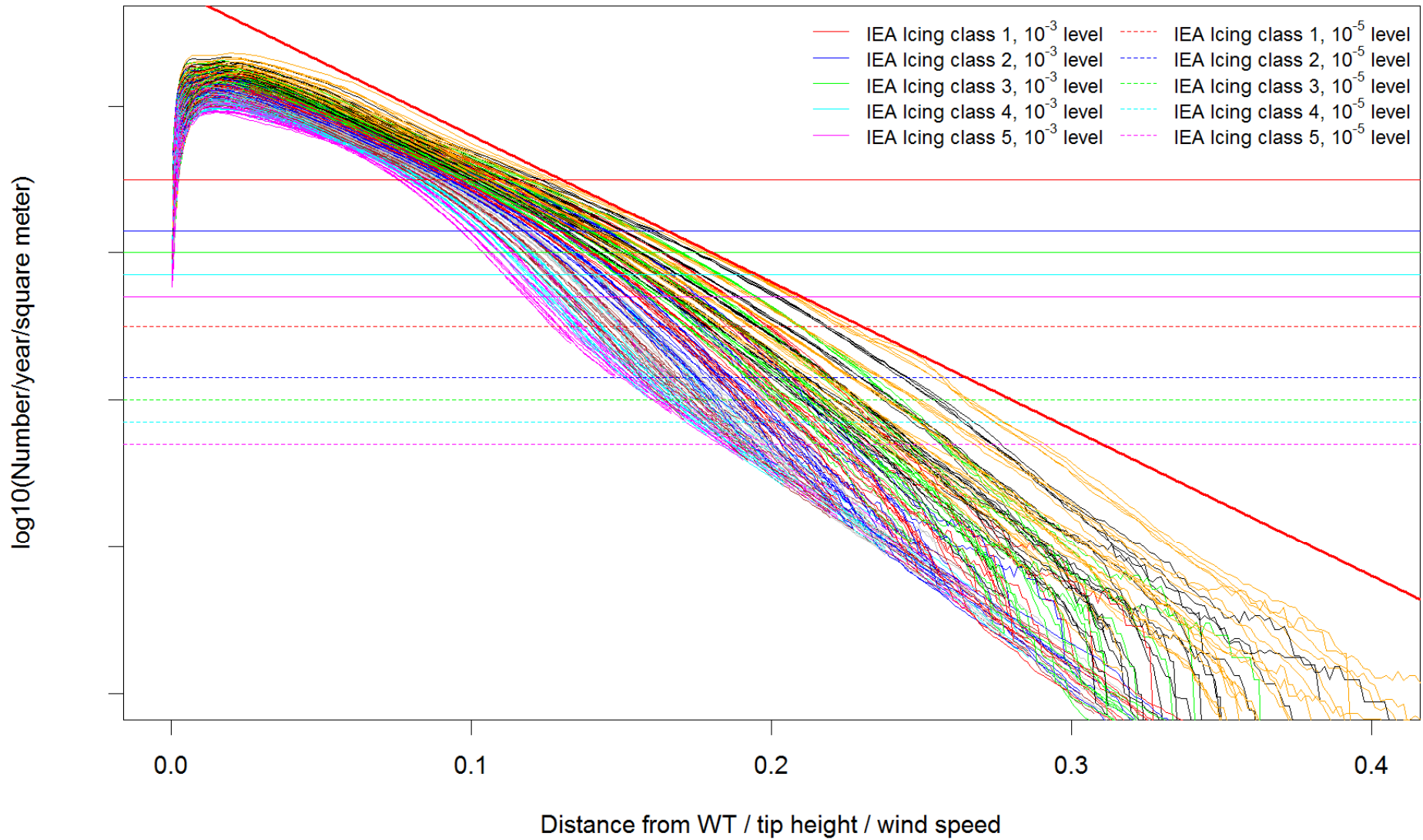
$V_{\text{avg}}$  ... average wind speed in "worst bin" [m/s]

$P_{\text{bin}}$  ... frequency of occurrence for "worst bin" [1]

### Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



# Impact probability of ice pieces, maximum over all directions, mean wind from 7 to 15 m/s



## Formulae for stand-off radii: iced WT in operation

- **$10^{-3} \text{ m}^{-2} \text{ year}^{-1}$**  for non-critical infrastructure and usage scenarios  
(also used for ice fall warning signs/warning lights)

$$\frac{R_{\min}}{TH} = V_{\text{avg}} \frac{3 + \log(a) + \log(b) - 0.4}{20}$$

**$10^{-5} \text{ m}^{-2} \text{ year}^{-1}$**  corresponds to a LIRA (localized individual risk)  $< 10^{-6}$ , i.e. ice fall risk is no concern

$$\frac{R_{\min}}{TH} = V_{\text{avg}} \frac{5 + \log(a) + \log(b) - 0.4}{20}$$

$$a = \begin{cases} 1 & \text{for IEA icing class 1} \\ 5 & \text{for IEA icing class 2} \\ 10 & \text{for IEA icing class 3} \\ 20 & \text{for IEA icing class 4} \\ 40 & \text{for IEA icing class 5} \end{cases}$$

$$b = \max(1, P_{\text{bin}} \cdot 12)$$

$TH$  ... tip height

$V_{\text{avg}}$  ... average wind speed in "worst bin" [m/s]

$P_{\text{bin}}$  ... frequency of occurrence for "worst bin" [1]

**Radius for  $10^{-3} \text{ yr}^{-1} \text{ m}^{-2}$  – iced WT stopped / ice-fall**

|           |        | IEA Icing class |      |      |      |      |
|-----------|--------|-----------------|------|------|------|------|
|           |        | 1               | 2    | 3    | 4    | 5    |
| Mean wind | 7 m/s  | 0,53            | 0,73 | 0,81 | 0,90 | 0,98 |
|           | 8 m/s  | 0,61            | 0,83 | 0,93 | 1,02 | 1,12 |
|           | 9 m/s  | 0,68            | 0,94 | 1,04 | 1,15 | 1,26 |
|           | 10 m/s | 0,76            | 1,04 | 1,16 | 1,28 | 1,40 |
|           | 11 m/s | 0,84            | 1,14 | 1,28 | 1,41 | 1,54 |
|           | 12 m/s | 0,91            | 1,25 | 1,39 | 1,54 | 1,68 |
|           | 13 m/s | 0,99            | 1,35 | 1,51 | 1,66 | 1,82 |
|           | 14 m/s | 1,06            | 1,46 | 1,62 | 1,79 | 1,96 |
|           | 15 m/s | 1,14            | 1,56 | 1,74 | 1,92 | 2,10 |

**Radius for  $10^{-5} \text{ yr}^{-1} \text{ m}^{-2}$  – iced WT stopped / ice-fall**

|           |        | IEA Icing class |      |      |      |      |
|-----------|--------|-----------------|------|------|------|------|
|           |        | 1               | 2    | 3    | 4    | 5    |
| Mean wind | 7 m/s  | 1,09            | 1,29 | 1,37 | 1,46 | 1,54 |
|           | 8 m/s  | 1,25            | 1,47 | 1,57 | 1,66 | 1,76 |
|           | 9 m/s  | 1,40            | 1,66 | 1,76 | 1,87 | 1,98 |
|           | 10 m/s | 1,56            | 1,84 | 1,96 | 2,08 | 2,20 |
|           | 11 m/s | 1,72            | 2,02 | 2,16 | 2,29 | 2,42 |
|           | 12 m/s | 1,87            | 2,21 | 2,35 | 2,50 | 2,64 |
|           | 13 m/s | 2,03            | 2,39 | 2,55 | 2,70 | 2,86 |
|           | 14 m/s | 2,18            | 2,58 | 2,74 | 2,91 | 3,08 |
|           | 15 m/s | 2,34            | 2,76 | 2,94 | 3,12 | 3,30 |

**Radius for  $10^{-3} \text{ yr}^{-1} \text{ m}^{-2}$  – iced WT operating / ice-throw**

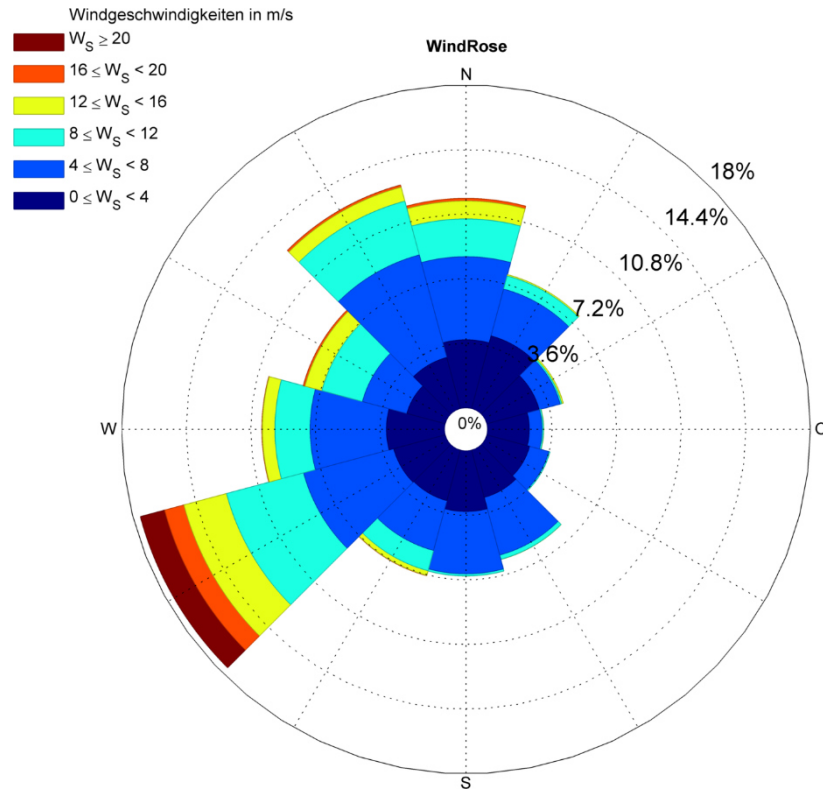
|           |        | IEA Icing class |      |      |      |      |
|-----------|--------|-----------------|------|------|------|------|
|           |        | 1               | 2    | 3    | 4    | 5    |
| Mean wind | 7 m/s  | 0,91            | 1,15 | 1,26 | 1,37 | 1,47 |
|           | 8 m/s  | 1,04            | 1,32 | 1,44 | 1,56 | 1,68 |
|           | 9 m/s  | 1,17            | 1,48 | 1,62 | 1,76 | 1,89 |
|           | 10 m/s | 1,30            | 1,65 | 1,80 | 1,95 | 2,10 |
|           | 11 m/s | 1,43            | 1,81 | 1,98 | 2,15 | 2,31 |
|           | 12 m/s | 1,56            | 1,98 | 2,16 | 2,34 | 2,52 |
|           | 13 m/s | 1,69            | 2,14 | 2,34 | 2,54 | 2,73 |
|           | 14 m/s | 1,82            | 2,31 | 2,52 | 2,73 | 2,94 |
|           | 15 m/s | 1,95            | 2,47 | 2,70 | 2,93 | 3,15 |

**Radius for  $10^{-5} \text{ yr}^{-1} \text{ m}^{-2}$  – iced WT operating / ice-throw**

|           |        | IEA Icing class |      |      |      |      |
|-----------|--------|-----------------|------|------|------|------|
|           |        | 1               | 2    | 3    | 4    | 5    |
| Mean wind | 7 m/s  | 1,61            | 1,85 | 1,96 | 2,07 | 2,17 |
|           | 8 m/s  | 1,84            | 2,12 | 2,24 | 2,36 | 2,48 |
|           | 9 m/s  | 2,07            | 2,38 | 2,52 | 2,66 | 2,79 |
|           | 10 m/s | 2,30            | 2,65 | 2,80 | 2,95 | 3,10 |
|           | 11 m/s | 2,53            | 2,91 | 3,08 | 3,25 | 3,41 |
|           | 12 m/s | 2,76            | 3,18 | 3,36 | 3,54 | 3,72 |
|           | 13 m/s | 2,99            | 3,44 | 3,64 | 3,84 | 4,03 |
|           | 14 m/s | 3,22            | 3,71 | 3,92 | 4,13 | 4,34 |
|           | 15 m/s | 3,45            | 3,97 | 4,20 | 4,43 | 4,65 |

Computed for a frequency of occurrence of  $1/12$  in wind direction bin with the highest wind speed, i.e.  $P_{\text{bin}} = 1/12$ .

# An example...



**Iced WT stopped / ice-fall**

Radius for  $10^{-3}$ :  $1.13 \cdot TH$   
 Radius for  $10^{-5}$ :  $1.90 \cdot TH$

**Iced WT operating / ice-throw**

Radius for  $10^{-3}$ :  $1.75 \cdot TH$   
 Radius for  $10^{-5}$ :  $2.72 \cdot TH$

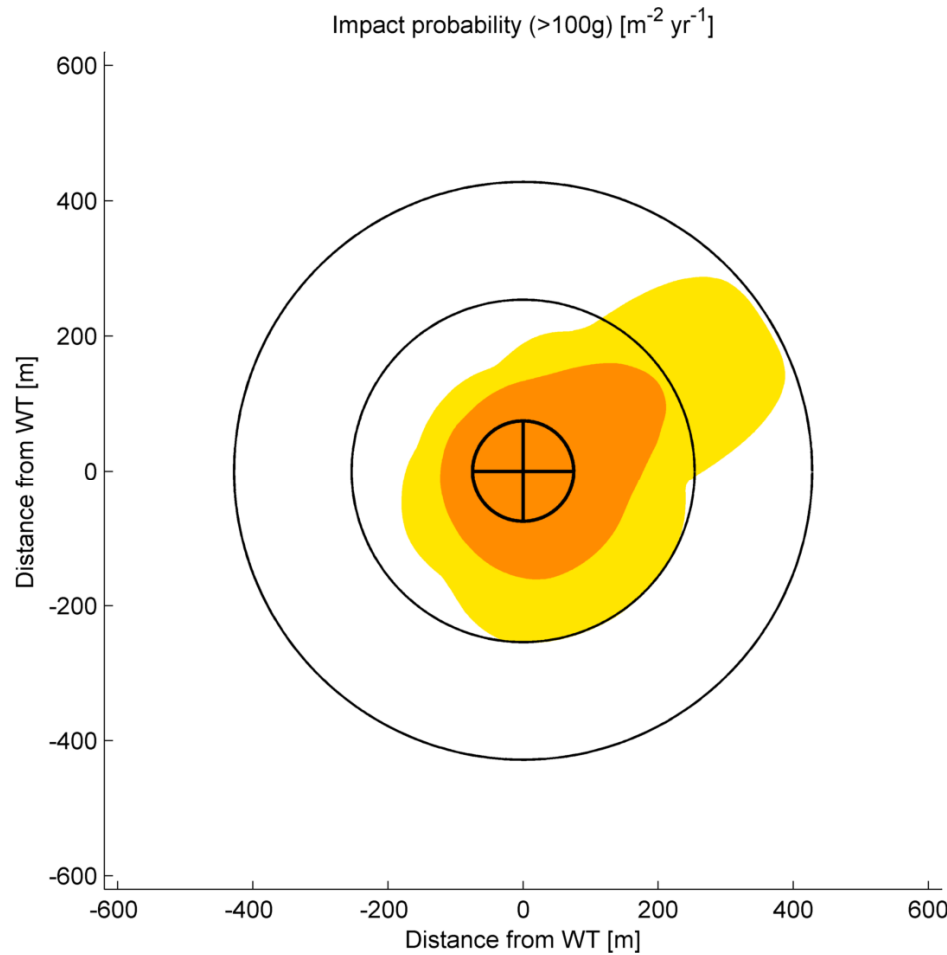
+ IEA Icing class 2

| Wind sector [°] | 0    | 30   | 60   | 90   | 120  | 150  | 180  | 210  | 240  | 270  | 300  | 330  |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Fraction [1]    | 0.12 | 0.08 | 0.04 | 0.03 | 0.04 | 0.06 | 0.07 | 0.07 | 0.18 | 0.10 | 0.08 | 0.13 |
| Mean wind [m/s] | 6.28 | 4.41 | 3.59 | 3.29 | 3.46 | 4.48 | 4.16 | 5.42 | 9.66 | 6.10 | 7.21 | 6.68 |

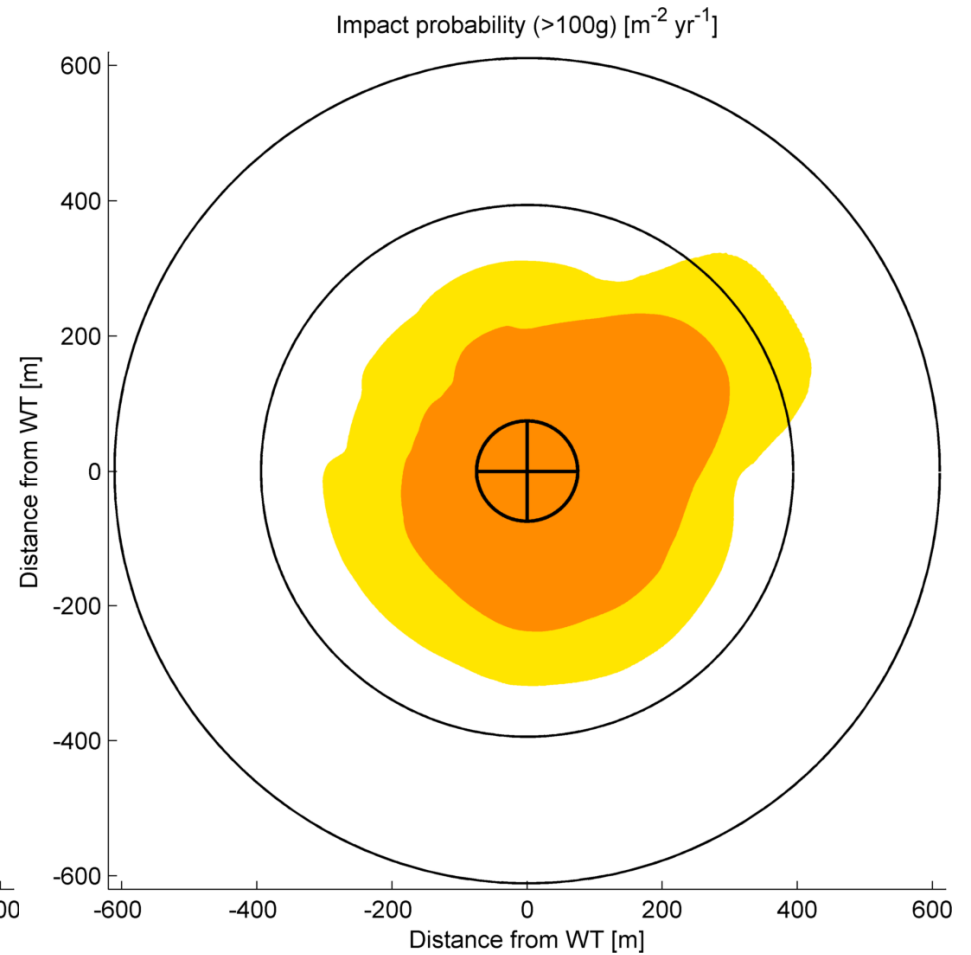


# An example...

## Iced WT stopped / ice-fall



## Iced WT operating / ice-throw



# Disclaimer

- Rough and simple
- No allowance of: wind directions, actual icing conditions, air density, actual WT operation, non-Rayleigh distribution, de-icing or anti-icing
- Ignores actual presence & frequentation of people
- Uncertainties in the ice-fall computations (A/m, ice shape,  $c_D$ , number and distribution of ice pieces)
- Nevertheless – useful **conservative** estimate:
  - Threat from falling ice pieces is largely overestimated (every ice piece above 100g causes a casualty)
  - Most wind directions are better than the “worst” direction
  - Most wind turbines are better than the “worst” turbine
  - Based on conservative usage scenarios

Thank you!